

Second-Order Optical Nonlinearity in Silicon Waveguides: Inhomogeneous Stress and Interfaces

Clemens Schrieffer, Federica Bianco, Massimo Cazzanelli, Mher Ghulinyan, Christian Eisenschmidt, Johannes de Boor, Alexander Schmid, Johannes Heitmann, Lorenzo Pavesi, and Jörg Schilling*

The lack of a dipolar second-order susceptibility ($\chi^{(2)}$) in silicon due to the centrosymmetry of its diamond lattice usually inhibits efficient second-order nonlinear optical processes in the silicon bulk. Recently, the deposition of stressed silicon nitride layers and the corresponding inhomogeneous strain in silicon lead to the demonstration of second harmonic generation and electro-optic modulation in strained silicon waveguides. However, the respective impact of the stress/strain gradient and the involved interfaces is not clear. Here, the influence of the stress and the stressing silicon nitride layer using second harmonic generation measurements in transmission is investigated. The results show that the enhancement of the second-order nonlinearity arises from a constructive superposition of stress-induced and interface-related effects. Particularly, the stress gradient in silicon breaks the symmetry of the crystal lattice, while positive fixed charges at the silicon/silicon nitride interface are responsible for a pronounced electric-field-induced-second harmonic (EFISH) contribution. These results demonstrate the impact of external factors for the creation of an effective $\chi^{(2)}$ in materials and open new perspectives for the use of second-order nonlinear optical processes in silicon photonics.

modulation using the linear electro-optic effect are not possible in silicon. On a fundamental level, this is caused by the centrosymmetry of the silicon crystal lattice, which results in a lack of a dipolar bulk $\chi^{(2)}$. Therefore, nonlinear active devices based on silicon are usually fabricated by exploiting its third-order nonlinearity $\chi^{(3)}$ ^[1] or combining various nonlinear materials with silicon.^[2–4] However, since silicon exhibits a strong two-photon absorption in the near infrared, the efficiency of these processes is limited. Of specific interest were also situations where the centrosymmetry of bulk the silicon crystal is naturally broken and a nonzero $\chi^{(2)}$ is induced, e.g., at free surface or an interface.^[5–8] This lead to efforts to deform the silicon lattice deliberately using inhomogeneous strain, e.g., through a deposition of a stressing layer.^[9–11] Recently, the stressing layer method was used to demonstrate second harmonic generation (SHG)^[12] and electro-optical modulation^[13,14] in strained silicon waveguides. In both cases, a silicon nitride (SiN_x) overlayer was used to induce the stress inside the silicon waveguide core. On the other hand, second-order nonlinearities were also observed from silicon nitride itself.^[15–19] In view of this, the different

1. Introduction

Although silicon photonics became an established technology in the last few years, nonlinear optical processes like difference frequency generation or ultrafast electro-optic

Dr. C. Schrieffer, Prof. J. Schilling
Centre for Innovation Competence SiLi-nano
Martin-Luther-University Halle-Wittenberg
Karl-Freiherr-von-Fritsch-Str. 3, 06120, Halle (Saale), Germany
E-mail: joerg.schilling@physik.uni-halle.de

Dr. F. Bianco, Dr. M. Cazzanelli, Prof. L. Pavesi
Nanoscience Laboratory
Department of Physics
University of Trento
via Sommarive 14
38123 Povo, Trento, Italy

Dr. F. Bianco
NEST, Istituto Nanoscienze-CNR and Scuola Normale Superiore
P.za S. Silvestro 12, 56127, Pisa, Italy

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M. Ghulinyan
Department of Advanced Photonics and Photovoltaics
Centre of Materials and Microsystems
Bruno Kessler Foundation, via Sommarive 18
38123 Povo, Trento, Italy

Dr. C. Eisenschmidt
Institute of Physics
Martin-Luther-University Halle-Wittenberg
Heinrich-Damerow-Str. 4, 06120, Halle (Saale), Germany

Dr. J. de Boor
Max Planck Institute of Microstructure Physics
Weinberg 2, 06120, Halle (Saale), Germany

A. Schmid, Prof. J. Heitmann
Institut für Angewandte Physik
TU Bergakademie Freiberg
Leipziger Str. 23, 09599, Freiberg, Germany



impact of interface, stress, and nature of the overlayer on the second-order nonlinearity is not clarified yet.

Here, we investigate the influence of the stress and the existence of a silicon nitride overlayer on the second-order nonlinear response of strained silicon waveguides. We will show a direct correlation of the integrated stress gradient in the silicon lattice (which is a measure of breaking of the centrosymmetry of the Si lattice) with the conversion efficiency for SHG. In addition, we discuss the impact of the silicon nitride cover layers and, specifically, of their interface with Si. For this purpose, a set of silicon-on-insulator waveguide samples was investigated under various conditions of mechanical stress.

2. Inhomogeneously Strained Si Waveguides

An overview of different sample structures is given in **Figure 1** and **Table 1**. All waveguides were fabricated from SOI wafers with a 2- μm -thick p-type device layer ($\rho = 2.4 \text{ Ohm cm}$, $N_A = 7 \times 10^{15} \text{ cm}^{-3}$). The set consists of a reference sample SiRef with uncoated 2- μm -thick Si-strip waveguides resting on a buried oxide layer of the same thickness. Furthermore, a sample SiO2 (Figure 1a), whose waveguides were covered with a layer of stressing thermal oxide, was produced. A comparison of the SH conversion efficiencies of both samples can be used to study the impact of stress on second-order nonlinearity without any effect from a SiN_x layer. Additionally, samples with silicon nitride overlayers of different stress conditions were produced. Sample SiN0 was completely covered with a thin, almost unstressed, SiN_x overlayer to investigate the influence of SiN_x layer alone, excluding any stress-related effects. To examine the combination of SiN_x and the stress effect, additional silicon-nitride-coated samples were processed with different stress extent, stress sign, and layer thicknesses.

To relate the second-order response measured in the nonlinear transmission experiments with the stress state of the waveguides, a finite element method (FEM) model was employed to estimate the stress tensor across the waveguide cross section, where a plane stress regime was assumed.^[20,21] **Figure 2** shows the distribution of the normal stress component σ_{xx} and the local stress gradient (arrows) for 10- μm -wide

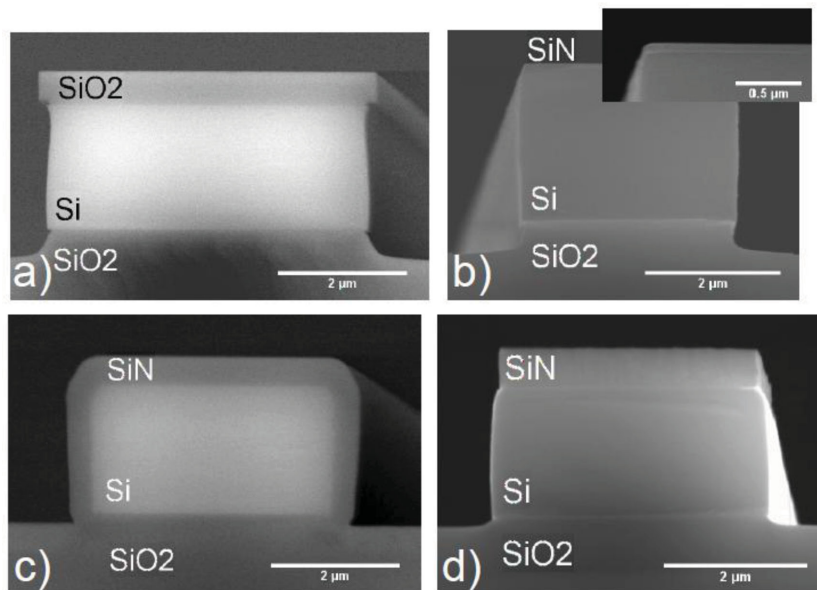


Figure 1. Scanning electron microscopy (SEM) images of the investigated waveguide facets. a) Covered with 500-nm SiO_2 (named SiO2), b) covered with 50-nm SiN_x layer (named SiN2), c) completely coated with 500-nm SiN_x (named SiN4), and d) covered with 500-nm SiN_x (named SiN1).

waveguides of different samples. Moreover, based on the sp^3 orbital models,^[9,10] a linear relationship between the second-order susceptibility $\chi^{(2)}$ and the stress gradient was assumed. A rigorous analysis would require the study of the influence of the local stress gradient on the local nonlinear optical properties of the waveguide core. However, the measurements of the SH light in transmission represent a nonsimple average of the local contributions along the waveguide cross section. Therefore, a total stress gradient was used to describe the overall stress inhomogeneity in the various samples. This was quantified by integrating the sum of the local gradients of the stress tensor components over the waveguide cross section as follows

$$\Sigma = \int \left(\left| \frac{\sigma_{xx}}{dx} \right| + \left| \frac{\sigma_{yy}}{dy} \right| + \left| \frac{\sigma_{xx}}{dy} \right| + \left| \frac{\sigma_{yy}}{dx} \right| + \left| \frac{\sigma_{xy}}{dx} \right| + \left| \frac{\sigma_{xy}}{dy} \right| \right) dA \quad (1)$$

A comparison of the stress distribution in the samples SiRef and SiN0 (Figure 2a and b) shows that the thin SiN_x cover layer has no influence on the stress inside the waveguide. On the contrary, the stress distribution is slightly affected by the stress in the underlying oxide layer that is created during the fabrication

Table 1. Parameters of the samples investigated here. The reported stress values were obtained by wafer bow measurement on complete wafers coated under identical conditions as the respective samples. Negative stress values describe compressively stressed layer resulting in tensile stress in the silicon and vice versa.

Sample layer	SiRef	SiO2 top	SiN0 compl.	SiN1 top	SiN2 top	SiN3 top	SiN4 compl.
Thickness [nm]	–	500	50	500	50	150	500
Layer stress [MPa]	–	–300	–7	+226	–880	+1200	+226
Integrated stress gradient Σ	–	3197	383	1535	1559	4504	821

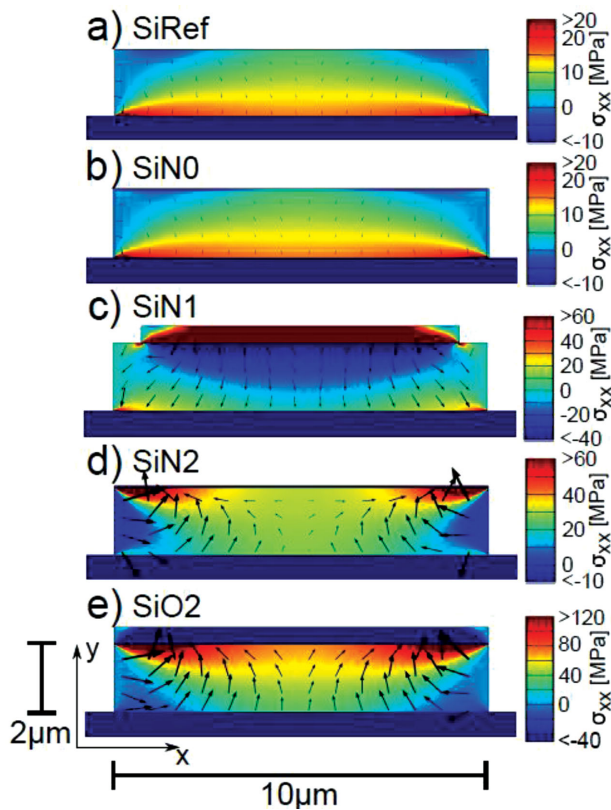


Figure 2. Simulated distribution of the stress component σ_{xx} along the cross section of 10- μm -wide waveguides for sample a) SiRef, b) SiN0, c) SiN1, d) SiN2, and e) SiO₂, as well as the resulting stress gradient (arrows).

of the SOI wafer ($\Sigma_{\text{SiRef}} = 436 \text{ N m}^{-1}$, $\Sigma_{\text{SiN0}} = 383 \text{ N m}^{-1}$).^[12,22] A stronger influence on the stress can be seen for the samples SiN1 and SiN2 with a stressed SiN_x layer on top (Figure 2c and d). Both samples show almost the same Σ ($\Sigma_{\text{SiN1}} = 1535 \text{ N m}^{-1}$, $\Sigma_{\text{SiN2}} = 1559 \text{ N m}^{-1}$). However, as both samples are coated with layers of different thickness and stress level, the local stress gradients differ strongly from each other. In Figure 2e, the stress distribution in the SiO₂-coated sample is shown exhibiting a strong total stress gradient of $\Sigma_{\text{SiO2}} = 3197 \text{ N m}^{-1}$.

To test the reliability of the employed FEM model for the calculation of the stress gradients, the stress distribution in a reference system has been modeled. The system consists of (111) oriented, laser written^[23] silicon grating structures, stressed by a 110-nm-thermal SiO₂ layer ($\sigma = -450 \text{ MPa}$). The numerical results were used to calculate artificial reciprocal space maps (RSM) for the Si-(111) reflex that were compared with experimental ones determined by high-resolution X-ray diffraction. In comparison to the diffraction pattern of the unstrained grating (Figure 3a), the strained grating exhibits a bending of its diffraction pattern in Q_z direction (Figure 3c).

The artificial RSMs were calculated using the kinematic diffraction theory.^[24] By this means, the amplitude of the field scattered by a single ridge can be expressed as^[25]

$$A_{\text{ridge}} = \sum_j F \exp \left[i \vec{Q} \times (\vec{r}_j + \vec{u}(\vec{r}_j)) \right] \quad (2)$$

The ridge is split into identical unit cells (10×10 atoms) with a form-factor F located at the position $\vec{r}_j + \vec{u}(\vec{r}_j)$. Here, $\vec{r}_j$ describes the position of the cell in the unstressed case, while $\vec{u}(\vec{r}_j)$ represents the additional displacement of the respective cell due to the local strain. The data for the position of the displaced unit cells were taken from the FEM model that was calculated using the actual parameters of the sample.

For the artificial RSM, the contribution of several ridges was taken into account by summing over the contribution of N single ridges separated by a lattice constant Γ :

$$A_{\text{total}} = A_{\text{ridge}} \times (1 + e^{iQ_z \Gamma} + \dots + e^{iQ_z N \Gamma}) = A_{\text{ridge}} \times \frac{e^{iQ_z (N+1)\Gamma} - 1}{e^{iQ_z \Gamma} - 1} \quad (3)$$

A comparison between the experimentally determined RSMs (Figure 3a,c) and calculated RSMs (Figure 3b,d) shows a good agreement for both cases – the stressed and unstressed geometries. This result proves that the FEM model is suitable to represent the actual stress distribution inside a stressed silicon waveguide and that the calculated integrated stress gradient discussed above is reliable.

3. Second Harmonic Generation from Si Waveguides

To investigate the second-order nonlinear optical properties of the different samples, the SH signal from 2-mm-long waveguides was measured in transmission using a tunable laser source with 100 fs-pulses at a wavelength of about 2200 nm (Figure 4). For one spectrum, an average of over 1000 single measurements was taken. To reduce the error when estimating the intensity of the SH peak, a Gaussian curve was fitted to the spectrum (Figure 4 Inset I). Inset II shows the typical linear dependence between the wavelengths of the SH and fundamental beams proving that indeed the SHG process was observed.

As it was not possible to estimate the exact SH intensity, no absolute $\chi^{(2)}$ values could be calculated. Instead, relative conversion efficiency η was determined, which allows a comparison of the second-order nonlinearities of the different samples measured under identical conditions. It is defined as

$$\eta = \frac{I_{2\omega}}{I_{\omega}^2} \quad (4)$$

that is the ratio between the SH intensity $I_{2\omega}$ and the squared excitation intensity I_{ω} . As the conversion efficiency was expected to be rather low, the effect of pump depletion was neglected here.

Figure 5 relates the estimated conversion efficiency η to the calculated total stress gradient Σ . To ensure confidence in the obtained values, η has been evaluated from at least three different waveguides with identical parameters. The error bars result from the maximum semi-dispersion of the determined values. For sample SiRef only a weak SH signal was generated. It is caused by contributions from the waveguide surfaces and the interface between silicon and native and buried SiO₂ layers, where the centrosymmetry is locally broken. A clear increase

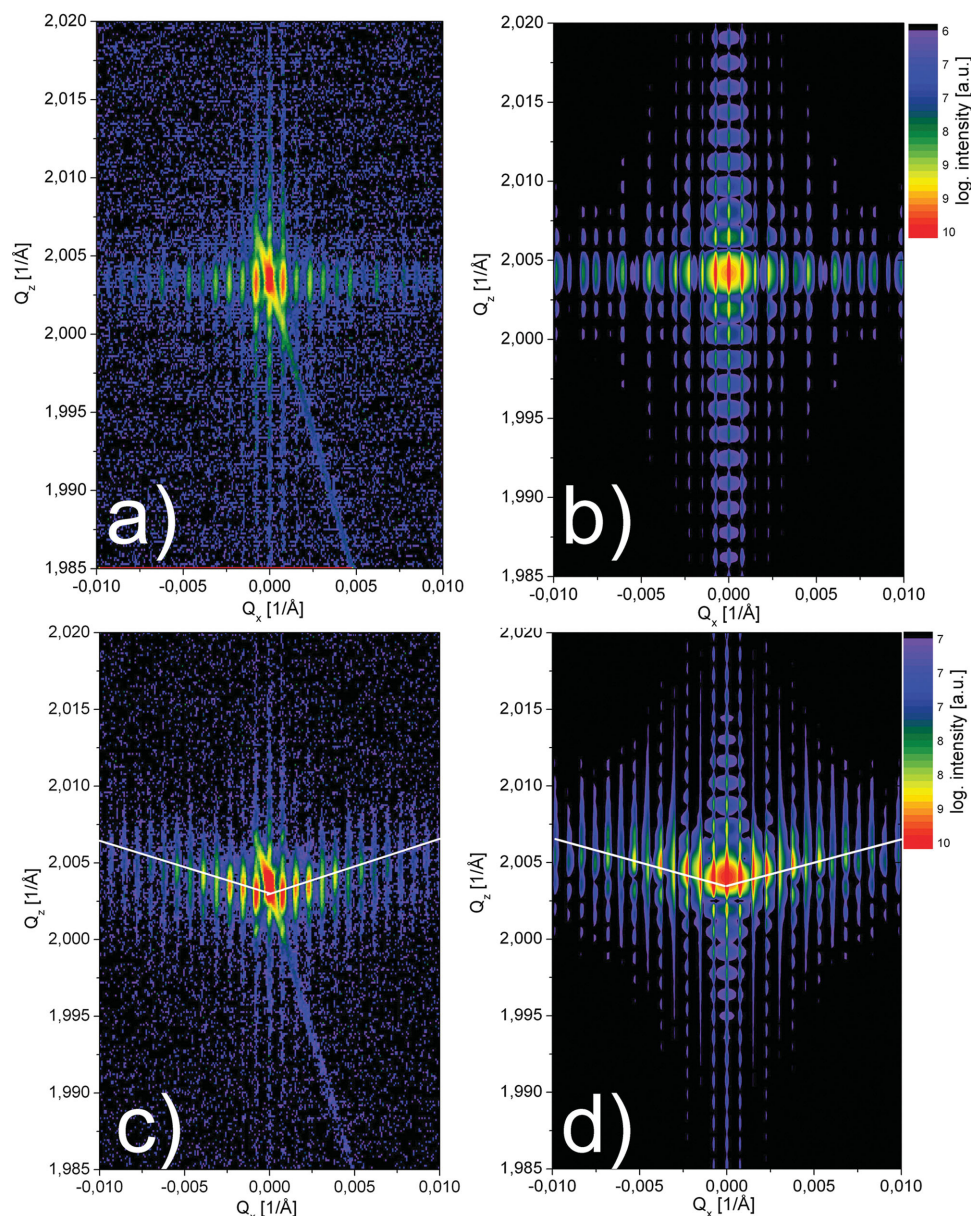


Figure 3. Comparison between experimentally (left) and numerically (right) determined reciprocal space maps (RSM) of the Si (111) reflex. In case of a stressing layer, the diffracted intensity shifts to higher Q_z values (white line). The additional feature in a) and c) represents the analyzer streak related to the X-ray setup. The strong agreement of the RSM confirms the accuracy of the FEM model used for the calculations.

of η was observed in the stressed SiO_2 -covered sample (SiO_2) (Figure 5). In this sample, the interface contributions can be considered comparable to the ones of sample SiRef, since also SiRef carries a natural oxide layer of a few nanometers thickness. Instead, analyzing the mechanical states of the two samples ($\Sigma_{\text{SiRef}} = 436 \text{ N m}^{-1}$ and $\Sigma_{\text{SiO}_2} = 3197 \text{ N m}^{-1}$), the sample SiO_2 shows a much larger total stress gradient, that indicates a stronger deformation of the Si–Si bonds in the crystalline lattice. The enhancement observed in the conversion efficiency can be thus attributed to the effect of the inhomogeneous stress inside the waveguide core that agrees with earlier statements.^[12]

When studying the conversion efficiency of the samples coated with a stressing silicon nitride layer (Figure 5), it can be

seen that η increases when the stress gradient increases. This is particularly obvious for the strongly stressed SiN_2 sample. It has the same film thickness, but a very different stress level compared with the quasi-unstressed SiN_0 sample. This confirms the existence of the stress related effect on $\chi^{(2)}$ also in the SiN_x -stressed samples.

To examine a possible nonlinear effect due to the SiN_x layer itself, the conversion efficiencies of SiRef and the silicon nitride covered (but quasi-unstressed) sample SiN_0 were compared. For SiN_0 , the conversion efficiency η is enhanced by a factor of approximately two compared with SiRef. This indicates an unexpectedly strong influence of the silicon nitride layer or its interface. In addition, one notes, that this contribution adds

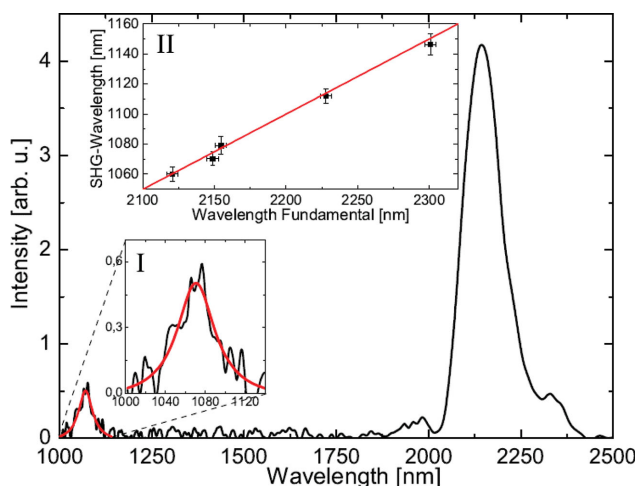


Figure 4. SHG measurements of a 10- μm -wide waveguide of sample SiO_2 showing peaks at the fundamental $\lambda_{\text{w}} = 2.14 \mu\text{m}$ and SH wavelengths $\lambda_{2\omega} = 1.07 \mu\text{m}$. The coupled average power of the fundamental beam was about 0.15 μW . Inset I shows the zoom of the SH peak, where the red line is the fitted Gaussian curve. Inset II shows the wavelength tunability of the SH signal. The red line is the expected relationship between $\lambda_{2\omega}$ and λ_{ω} .

constructively to the stress effect, leading to an overall stronger enhancement of the effective nonlinearity than in the case of sample SiO_2 . Additional support for the superposition of both effects (stress related and SiN_x related) is gained by adding the SiN_x layer contribution from sample SiN_0 to the conversion efficiency measured in sample SiO_2 . Interestingly, the resulting η value appears aligned with the trend observed for the other stressed SiN_x -covered samples (diamond marker in Figure 5).

The origin of the strong SH signal in the quasi-unstressed sample SiN_0 is indeed puzzling. From the presented results, we conclude that the reason for its increased SH-intensity has to lie within the SiN_x layer or the SiN_x/Si interface. However,

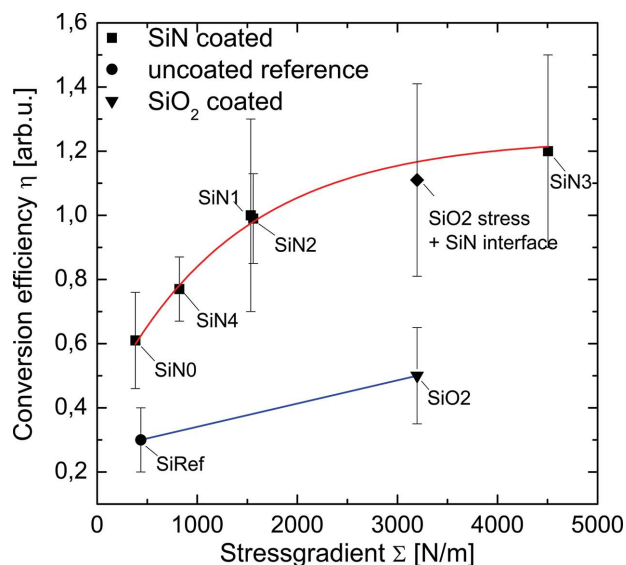


Figure 5. Dependence of the experimentally determined nonlinear conversion efficiency η on the total stress gradient Σ for 10- μm -wide waveguides under different stressing conditions. The lines are guides to the eye.

results and interpretations from literature are not conclusive in this respect. Previous studies on second-order nonlinearity in silicon nitride reported the observation of a strong SHG from PECVD silicon nitride films grown on fused silicon oxide substrate,^[16] where the nonlinearity was assigned to a SiN_x bulk origin. On the other hand, an interface-induced $\chi^{(2)}$ was reported in thin-film Bragg reflectors fabricated in various compositions of amorphous silicon nitride,^[17] in high-quality amorphous silicon nitride ($a\text{-Si}_{1-x}\text{N}_x\text{:H}$) Fabry–Perot microcavities^[18] and in multilayer silicon-oxy-nitride (SiON) waveguides.^[19] Furthermore, a SH signal was generated in PECVD silicon nitride ring resonators,^[15] where the nonlinearity was attributed to the interface between the silicon nitride and the silicon oxide. In our case, however, the conversion efficiency does not seem to depend on the layer thickness of SiN_x : Sample SiN_1 (500 nm SiN_x) and Sample SiN_2 (50 nm SiN_x) show basically the same conversion efficiency. Thus, a contribution from a silicon nitride bulk $\chi^{(2)}$ seems negligible in our case, so that the Si/SiN_x interface remains as possible source for additional SHG enhancement.

4. Charge State and Electric Field at the Interface

To clarify the impact of the SiN_x/Si interface, we investigated the charge state of the SiN_x and SiO_2 layers. For this purpose, Capacitance–Voltage (C – V) measurements were carried out at SiN_x layers and a SiO_2 layer, which were deposited in the same way as the waveguide samples investigated here. **Figure 6** shows the C – V curves for the sample coated with 57 nm of quasi-unstressed SiN_x layer (representing the conditions at waveguide sample SiN_0) and for a 482-nm-thick thermal oxide layer (representing the conditions at waveguide sample SiO_2). Both curves show a steep increase in capacitance when a sufficient negative potential is applied to the top aluminum contact. This corresponds to the transition from depletion toward accumulation of charges in the Si at the $\text{Si}/\text{insulator}$ interface. However, the onset of this rise is quite different for both samples. Especially for the SiN_x -coated sample, a strong negative potential

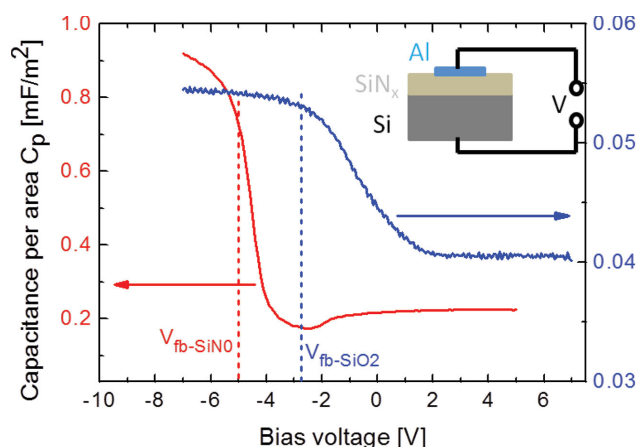


Figure 6. C – V measurement for SiN_x and SiO_2 layers on a 2.5 Ohm cm^{-1} p-type Si wafer. Red (left scale): 57-nm-thick quasi-unstressed (-7 MPa) SiN_x layer, blue (right): 482-nm thermal SiO_2 . Inset: measurement geometry with Al top contact on SiN_x or SiO_2 layer on Si wafer.

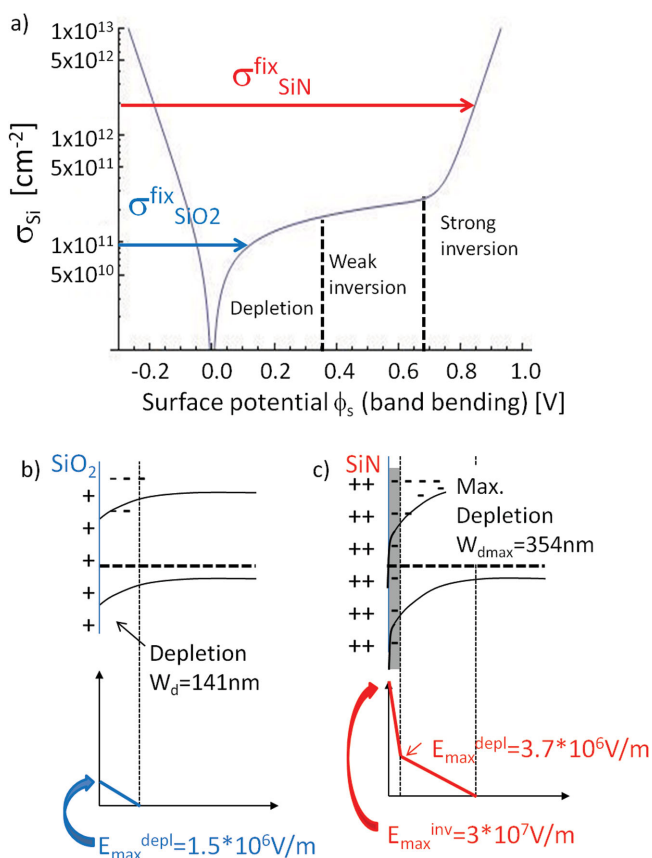


Figure 7. Charge conditions at the Si/insulator interface a) charge on the Si side of the interface depending on the surface potential. The lower level fixed positive charges in the oxide causes only a depletion layer in the Si, while the higher charge density in the nitride drives the Si in inversion b) band bending near the SiO₂/Si interface for depletion. The “+” indicate the positive fixed charges in the oxide, while the “-” are the resulting negative counter charges in the depletion layer in the Si. c) Band bending near the SiN_x/Si interface for inversion. After a densely charged inversion layer (gray-shaded area), a depletion layer of maximum width 350 nm follows.

of around -4 V is necessary to start accumulation. This is already a qualitative indication that the SiN_x layer carries a lot of fixed positive charges. Following the classic procedure for the evaluation of these C–V curves (see the Supporting Information Section A and ref. [26]), the areal density of these positive fixed charges can be derived from the position of the flat bend voltage V_{fb} and was determined to $\sigma_{fix-SiN0} = 2 \times 10^{12} \text{ cm}^{-2}$ and $\sigma_{fix-SiO2} = 9.9 \times 10^{10} \text{ cm}^{-2}$ for the SiN_x layer and the SiO₂ layer, respectively. The high concentration of positive fixed charges in the SiN_x layer is remarkable. Furthermore, we conclude that the majority of these charges must be located close to the Si/SiN_x interface since C–V measurements for the SiN_x layers with 500 nm thickness (representing the samples SiN1 and SiN4) resulted in a similar overall areal charge density of $\sigma_{fix-SiN1} = 1.1 \times 10^{12} \text{ cm}^{-2}$, although the layer was an order of magnitude thicker than the SiN0-like sample (see Supporting Information Section B). These positive fixed charges will drive the holes in the p-type silicon away from the interface leading to majority carrier depletion. An effective negative space charge builds up in the Si, which has the same value as the fixed charges in the SiN_x or SiO₂ layer.

From the knowledge of the p-type doping level ($7 \times 10^{15} \text{ cm}^{-2}$), the relationship between the surface potential ϕ_s at the interface and the areal charge density within the silicon can be derived (Figure 7a). For charge densities which correspond to $\sigma_{fix-SiO2}$ the silicon is in depletion, which results in a maximum electric field of $E_{max}^{int} = 1.5 \times 10^4 \text{ V cm}^{-1}$ at the interface. Assuming a constant negative charge density within the depletion layer of $N_A = 7 \times 10^{15} \text{ cm}^{-2}$ (negatively charge acceptors), a moderate depletion width of 141 nm results (Figure 7b). The much higher positive fixed charge density of the nitride layers on the other hand leads to a considerably stronger electric field at the interface: $E_{max}^{int} = 3 \times 10^5 \text{ V cm}^{-1}$ (Figure 7c). This causes a densely charged inversion layer at the interface with a width of about 10 nm. Although the electric field drops fast in this inversion layer, a sizeable field of the order of 10^4 V cm^{-1} still penetrates up to 350 nm deep into the silicon, which corresponds to the maximum width of the adjacent depletion layer.

The DC electric field in depletion and inversion layers has an impact on the optical properties. It breaks the centrosymmetry in the silicon band structure, so that electric-field-induced-second harmonic generation (EFISH) can emerge from there. Since the DC electric fields in the inversion and depletion layer of the nitride-covered samples are considerably higher than in the oxide-coated case, a much stronger EFISH-effect is expected for the SiN_x-coated Si waveguides. Furthermore, the penetration depth of the DC electric fields into the silicon is larger for the SiN_x-coated samples, since its depletion width is more than double the depletion width for the oxide-coated samples.

Note, that the EFISH-effect is a known effect in silicon and was already thoroughly investigated at MOS capacitors,^[27–30] where a voltage was applied externally across the MOS-structure generating electric fields of the order of 10^5 V cm^{-1} in the silicon space charge layer. As a result, a manifold enhancement of the SH signal was observed in reflection from the dielectric/semiconductor interface of the MOS structure.

We suggest that in our waveguides the same EFISH effect contributes to the SHG signal measured in transmission, but that the electric field is internally created by the fixed positive charges within the coatings.

The EFISH effect is actually a third-order nonlinear effect, which is based on the $\chi^{(3)}$ of a material and the application of a DC electric field. The nonlinear polarization P^{NL} can be written as^[31]

$$P^{NL} = 3\epsilon_0\chi^{(3)}E_{DC}E^2(\omega) \quad (5)$$

When $E(\omega)$ represents the oscillating electric field of the pump light, the resulting nonlinear polarization will have a component at 2ω —the SHG signal. To compare the possible strength of this quasi-second-order nonlinearity with the classic values for $\chi^{(2)}$ of other materials, a quasi- $\chi^{(2)}$ ($\chi_{quasi}^{(2)}$) can be defined in our case as

$$\chi_{quasi}^{(2)} = \chi^{(3)}E_{DC} \quad (6)$$

A $\chi^{(3)} = 3.82 \times 10^{-11} \text{ m}^2 \text{ V}^{-2}$ for silicon at pump wavelengths around 2.2 μm can be derived from the silicon Kerr coefficient

$n_2 = 9 \times 10^{-14} \text{ cm}^2 \text{ W}^{-1}$, which was determined by a z-scan technique.^[32] From this a maximum $\chi_{\text{quasi}}^{(2)} = 11.4 \text{ pm V}^{-1}$ is obtained for the maximum DC electric field of $3 \times 10^7 \text{ V m}^{-1}$ at the SiN_x/Si interface. For the lower electric field at the SiO_2/Si interface, Equation (6) yields $\chi_{\text{quasi}}^{(2)} = 0.6 \text{ pm V}^{-1}$. Although these numbers can only represent estimates [since they are based on the n_2 values, which were determined for the case when all three electric field factors in Equation (5) have the same high frequency ω], they nevertheless indicate that a quasi- $\chi^{(2)}$ with values on the order of classic second-order nonlinear materials can be generated by the observed DC electric fields.

Since the areal charge density is similar for all nitride-coated samples, we might conclude that all our investigated SiN_x layers experience the same high level of the EFISH effect. This further supports our earlier assumption that we can add the same offset in SHG enhancement (now known as EFISH) to the conversion efficiencies of all SiN_x -covered samples in Figure 5.

With this, we could show that inhomogeneous strain and interface charges are both possible sources for enhanced SHG in silicon waveguides. A further increase in inhomogeneous strain (represented by even stronger stress/strain gradients) and highly charged interfaces will be a way to increase the generated second-order nonlinearity further.

When our results are compared with the relevant literature on SHG reflection measurements on MOS structures, it has to be emphasized that in our case pump light and SH light are in the infrared with photon energies even below the indirect Si bandgap ($\lambda_{20} > 1100 \text{ nm}$). The observed resonant enhancement of the SHG, when the photon energy of the SH radiation approaches the direct bandgap of Si,^[29,30] does, therefore, not appear in our experiments. Furthermore, effects like the shift of the flatband voltage due to the screening of the electric field by photoexcited free carriers^[33] can also be neglected in our case, as the low energy IR photons of pump and SH radiation cannot excite electron hole pairs. On the other hand, contributions to the SHG from stress-induced changes to the second-order bulk quadrupole susceptibility^[34] cannot be totally excluded, since the observed rise of the SHG efficiency with the integrated stress gradient could partly be caused by the overall rise of the stress/strain level in Si too. Further studies, which focus on a comparison of the SHG from homogeneously and inhomogeneously strained waveguide structures, are necessary to clarify this point.

5. Conclusion

The influences of the inhomogeneous stress and the presence of a silicon nitride layer on the second-order nonlinearity in silicon waveguides could be separated. Both schemes enhance the nonlinear optical response of the waveguides. While the stressed layers create an inhomogeneous strain field within the silicon and break its centrosymmetry in this way, the enhancement due to the SiN_x alone was attributed to a high level of fixed positive charges close to the Si/SiN_x interface, which lead to a strong electric field in the silicon near the interface and cause a pronounced EFISH contribution. It was also found, that both contributions add up constructively, which allows the combination of both methods to further enhance the effective nonlinearity of the waveguides in the future.

6. Experimental Section

Sample Preparation: The Si-reference waveguide was fabricated in a classic way by first defining the strip waveguide photolithographically on the Si-device layer of the SOI substrate and then etching the wafer in an inductively coupled reactive ion etching system (ICP-RIE "Plasmalab 100") using a $\text{SF}_6/\text{C}_4\text{H}_8$ gas mixture. The remaining resist was finally removed in an oxygen plasma. The oxide-covered Si waveguides were fabricated by first thermally oxidizing the SOI substrates at 1050°C for 1 h in water vapor (wet oxidation), thereby growing a 500-nm-thick silicon dioxide layer. Afterward the waveguides were structured as before forming the oxide-covered waveguides. The SiN_x -covered samples SiN_0 , SiN_1 , SiN_2 , and SiN_4 were fabricated by depositing the SiN_x layers using dual frequency sputtering on the SOI. During this sputter process, the stoichiometry of the deposition plasma remains constant but the radio frequency is modulated allowing the deposition of differently stressed layers. For the samples SiN_1 and SiN_2 , the nitride layer was deposited before the waveguide etching, while for the samples SiN_0 and SiN_4 first the waveguides were structured (similar like SiRef) and afterward the SiN_x was deposited leading to a more conformal SiN_x coating for SiN_0 and SiN_4 .

The waveguides of SiN_3 were first etched and afterwards covered by SiN_x using a low-pressure chemical vapor deposition process (LPCVD), leading to the conformal coating of highest stress.

Measurement of Second Harmonic Generation: The pump laser was coupled in and out of the waveguides using gold-coated reflecting mirror objectives. The laser spot size at the entrance facet of the waveguide was about $4 \mu\text{m}$ in diameter and the pump laser was polarized horizontally. By imaging first, the transmitted pump beam onto an IR Vidicon Camera (sensitive in the spectral range from 0.75 to $2.25 \mu\text{m}$), the best waveguide coupling and the predominant excitation of the fundamental TE_{00} waveguide mode was assured. This coupling results in insertion losses on the order of ≈ 12 – 15 dB . Subsequently, the signal from the waveguide was recorded by a Fourier transform infrared spectrometer (FTIR) equipped with a LN_2 -cooled InSb-detector, which allowed simultaneous recording of the signal at fundamental and SH wavelengths. The linear propagation losses for the SH-wavelength were only 1 – 3 dB cm^{-1} , since for the SH-wavelengths $> 1100 \text{ nm}$ investigated by us interband absorption does not yet occur and the linear waveguide losses are governed by free carrier intraband absorption and scattering from waveguide surface roughness.

C–V Measurements: Si bulk wafers with a similar doping level ($7 \times 10^{15} \text{ cm}^{-3}$) as the SOI waveguides were used and SiN_x layers as well as a wet-thermal oxide layer were deposited/grown under the same conditions as the waveguide samples. Afterwards aluminum contact pads with different rectangular areas ranging from $350 \mu\text{m} \times 350 \mu\text{m}$ to $950 \mu\text{m} \times 950 \mu\text{m}$ were fabricated using photolithography and a lift-off process. Subsequently, the large area samples (ca. 10 cm^2) were placed on a metal plate, which functioned as the bottom contact, while a needle contact was applied at the Al pads. The C–V curves were measured with an LCR-meter at several ac frequencies. Here, only the 1 MHz measurements are shown.

Supporting Information

Supporting Information is available from the Wiley Online Library or from the author.

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